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OPTIMUM COPLANAR FLIGHTS BETWEEN ORBITS

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[USSR]

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3. OPTIMUM COPLANAR FLIGHT BETWEEN ORBITS

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5.  
by S. N. KirpichnikovABSTRACT

The optimum coplanar flight between assigned orbits is considered in this work. It is realized with the aid of a boost with minimum value of characteristic velocity. This ensures the minimum fuel consumption. It is postulated that the motion on all orbits, whether initial, intermediary or final, is Keplerian. Two cases are considered, the flight between circular orbits and that between orbits of small eccentricity. The cases of flight without taking into account the motion time, and those when account of concrete motion time is taken, are dealt with separately.

In the first approximation it is possible to relate these problems to those of space probes to Mars, Venus and other planets of the solar system, as, for example, the flight of the interplanetary automatic station "Mars-1". The problems linked with AES orbit variations, and, in particular, the coplanar problem of hitting another satellite from an assigned AES orbit by means of a unique impulse (boost), minimum from the standpoint of mass consumption, also belong to that category.

\* \* \*

#1. - MINIMUM OF THE FUNCTION DEFINED BY A FAMILY OF VARIABLES  
WITH TWO DISCONTINUITIES

Let  $y_i = y_i(x), i = 1, 2, \dots, n$  (1.1)

be the unknown function of an independent variable  $x \in [a, b]$ , continuous

everywhere with the partial derivatives with the exception of two ordinary discontinuities of the first kind at two points  $x_1, x_2$ , unknown beforehand.

Whenever they are continuous, the functions (1,1) must everywhere satisfy the system of differential equation

$$\frac{dy_i}{dx} = f_i(x, y_j), \quad i, j = 1, 2, \dots, n, \quad (1,2)$$

assuming at the same time that the conditions of theorem existence and uniqueness are fulfilled.

We shall introduce the following denotations:

$$\left. \begin{aligned} y_{i1a} &= y_i(a), & y_{i1} &= y_i(x_1 + 0), & y_{i22} &= y_i(x_2 + 0), \\ y_{i11} &= y_i(x_1 - 0), & y_{i2} &= y_i(x_2 - 0), & y_{i2b} &= y_i(b). \end{aligned} \right\} \quad (1,3)$$

For the values of variables (1,1) at end points  $a, b$  and at points of discontinuity  $x_1, x_2$  there is the system of conditions

$$\begin{aligned} \widetilde{\varphi}_s(a, b, x_1, x_2, y_{i1a}, y_{i11}, y_{i1}, y_{i2}, y_{i22}, y_{i2b}) &= 0, \\ s &= 1, 2, \dots, r < 3n + 4. \end{aligned} \quad (1,4)$$

Let us consider the assigned function

$$g = \widetilde{g}(a, b, x_1, x_2, y_{i1a}, y_{i11}, y_{i1}, y_{i2}, y_{i22}, y_{i2b}). \quad (1,5)$$

Functions (1,1) must be found, satisfying both, the differential equations (1,2) and the conditions (1,4), and also the end points  $a, b$  and the discontinuity points  $x_1, x_2$  so that the function  $g$  have a minimum.

We shall provide the solution of the variational problem posed, if the general solution of the system (1,2) is known:

$$\Phi_i = y_i - y_i(x, c_j) = 0, \quad i, j = 1, 2, \dots, n, \quad (1,6)$$

where  $c_j$  are arbitrary constants. We shall estimate, that the functions  $\Phi_i$  have continuous partial derivatives over all the arguments, and that the determinant

$$\left| \frac{\partial \Phi_i}{\partial c_j} \right| \neq 0. \quad (1,7)$$

Denoting

$$\left. \begin{aligned} y_{i1}(x, c_{j1}) &= y_i(x) & \text{at } x \in [a, x_1], \\ y_i(x, c_j) &= y_i(x) & \text{at } x \in [x_1, x_2], \\ y_{i2}(x, c_{j2}) &= y_i(x) & \text{at } x \in [x_2, b], \end{aligned} \right\} \quad (1,8)$$

we have:

$$\left. \begin{aligned} y_{i1a} &= y_{i1}(a, c_{j1}), & y_{i11} &= y_i(x_1, c_j), & y_{i22} &= y_{i2}(x_2, c_{j2}), \\ y_{i11} &= y_{i1}(x_1, c_{j1}), & y_{i2} &= y_i(x_2, c_j), & y_{i2b} &= y_{i2}(b, c_{j2}). \end{aligned} \right\} \quad (1,9)$$

As a consequence of correlations (1,9), the conditions (1,4) will be

$$\varphi_s(a, b, x_1, x_2, c_{j1}, c_j, c_{j2}) = 0, \quad (1,10)$$

and the function (1,5) will take the form

$$g = g(a, b, x_1, x_2, c_{j1}, c_j, c_{j2}). \quad (1,11)$$

The earlier-formulated problem is reduced in this case to the equivalent problem of finding the minimum of the function of finite number of variables. What is required is the determination of the function (1,8), i.e. the finding of the value of arbitrary constants  $c_{j1}, c_j, c_{j2}$  and of the points  $a, b, x_1, x_2$ , satisfying the system of conditions (1,10) in such a way, that the function (1,11) have a minimum.

If at extreme values of arguments the functions (1,10) and (1,11) have continuous partial derivatives of the first order, then, as is well known [1], it is necessary that there exist such constant multipliers  $\lambda_1, \lambda_2, \dots, \lambda_r$  for which the conditions

$$\frac{\partial g}{\partial a} + \sum_{s=1}^r \lambda_s \frac{\partial \varphi_s}{\partial a} = 0, \quad \frac{\partial g}{\partial b} + \sum_{s=1}^r \lambda_s \frac{\partial \varphi_s}{\partial b} = 0, \quad (1,12)$$

$$\frac{\partial g}{\partial x_1} + \sum_{s=1}^r \lambda_s \frac{\partial \varphi_s}{\partial x_1} = 0, \quad \frac{\partial g}{\partial x_2} + \sum_{s=1}^r \lambda_s \frac{\partial \varphi_s}{\partial x_2} = 0, \quad (1,13)$$

$$\frac{\partial g}{\partial c_{j1}} + \sum_{s=1}^r \lambda_s \frac{\partial \varphi_s}{\partial c_{j1}} = 0, \quad \frac{\partial g}{\partial c_{j2}} + \sum_{s=1}^r \lambda_s \frac{\partial \varphi_s}{\partial c_{j2}} = 0, \quad (1,14)$$

$$\frac{\partial g}{\partial c_j} + \sum_{s=1}^r \lambda_s \frac{\partial \varphi_s}{\partial c_j} = 0, \quad j = 1, 2, \dots, n. \quad (1,15)$$

are fulfilled. Moreover, if by its arguments, the rank of the matrix

constituted of partial derivative functions  $\varphi_s(a, b, x_1, x_2, c_{j1}, c_j, c_{j2})$  is equal to  $r$ , the multipliers  $\lambda_1, \lambda_2, \dots, \lambda_r$  are unique.

Therefore a system of necessary conditions (1,12) — (1,15), (1,10) is obtained from  $3n + r + 4$  equations with the very same number of unknowns  $a, b, x_1, x_2, c_{j1}, c_j, c_{j2}, \lambda_s$  for the solution of the problem set up.

In the case of a problem with fixed ends, i. e. at values  $a, b, y_{ha}, y_{hb}$  fixed beforehand, the constants  $c_{j1}, c_{j2}$  will be found unilaterally, as a consequence of the correlation (1,7), and the equations (1,12) and (1,14) in the system of indispensable conditions (1,10) and (1,12) — (1,15), must be rejected.

## #2.- SYSTEM OF NECESSARY CONDITIONS IN CASE OF A FLIGHT WITHOUT TAKING INTO ACCOUNT THE MOTION TIME IN ORBITS

We shall define the complanar Keplerian orbits by the following elements:

$$p = \frac{1}{\sqrt{a(1-e^2)}}, \quad q = \frac{e}{\sqrt{a(1-e^2)}}, \quad \omega. \quad (2,1)$$

where  $a, e, \omega$  are respectively the major semi-axis, the eccentricity and the angular distance from the pericenter to the polar axis. The polar angle  $\vartheta$  will be taken as the independent variable.

Assume that the initial orbit has the elements  $p_1, q_1, \omega_1$  and the final one —  $p_2, q_2, \omega_2$ . The impulse, as a result of which we obtain the intermediate orbit of the flight with the elements  $p, q, \omega$ , takes place at the time when the polar angle is  $\vartheta_1$ . At  $\vartheta = \vartheta_2$  this orbit will intersect the final orbit. We now must find the flight orbit for assigned initial and final orbits, i. e. its elements  $p, q, \omega$  and also the angles  $\vartheta_1$  and  $\vartheta_2$ , in such a way, that the value of the characteristic velocity of the initial impulse be at the minimum.

Since the elements of the boundary orbits  $p_1, q_1, \omega_1$  and  $p_2, q_2, \omega_2$  are assigned, we shall utilize for the system of necessary conditions the equations (1,13) and (1,15), in which  $x_1$  and  $x_2$  play the role of  $\vartheta_1$  and  $\vartheta_2$ , and  $p_1, q_1, \omega_1, p, q, \omega, p_2, q_2, \omega_2$  are respectively taken for

At elements' discontinuity points the following conditions must be fulfilled:

$$\varphi_1 = p^2 + pq \cos(\vartheta_1 - \omega) - p_1^2 - p_1 q_1 \cos(\vartheta_1 - \omega_1) = 0, \quad (2,2)$$

$$\varphi_2 = p^2 + pq \cos(\vartheta_2 - \omega) - p_2^2 - p_2 q_2 \cos(\vartheta_2 - \omega_2) = 0, \quad (2,3)$$

which, as a consequence of correlations

$$\frac{1}{a(1-e^2)} + \frac{e \cos(\vartheta - \omega)}{a(1-e^2)} = p^2 + pq \cos(\vartheta - \omega) \quad (2,4)$$

denote the continuity of the values of radius-vectors at these points.

We shall use for the function  $g$

$$g = \frac{1}{2K^2} [(V_r - V_r)^2 + (V_\theta - V_\theta)^2], \quad (2,5)$$

where  $V_r$ ,  $V_\theta$  and  $V_{r_1}$ ,  $V_{\theta_1}$  are respectively the radial and transverse vector components at the point of the initial impulse, prior and after the latter, and

$$K = k\sqrt{M}. \quad (2,6)$$

In the latter correlation  $k$  is the gravitational constant,  $M$  is the mass of the central body  $M$ . We neglect the mass of the rocket by comparison with that of the central body, and also the masses of planets by comparison with that of the Sun, whenever we analyze interplanetary flights.

For velocity components, we have:

$$V_r = \frac{Ke \sin(\vartheta_1 - \omega)}{\sqrt{a(1-e^2)}} = Kq \sin(\vartheta_1 - \omega), \quad V_\theta = \frac{K\sqrt{a(1-e^2)}}{r_1} = \frac{K}{pr_1} \quad (2,7)$$

and analogously

$$V_{r_1} = Kq_1 \sin(\vartheta_1 - \omega_1), \quad V_{\theta_1} = \frac{K}{p_1 r_1}, \quad (2,8)$$

where  $r_1$  is the value of the radius-vector at time of initial impulse.

Taking advantage of correlations (2,7), (2,8) and of dependences

$$r_1^{-1} = p^2 + pq \cos(\vartheta_1 - \omega) = p_1^2 + p_1 q_1 \cos(\vartheta_1 - \omega_1), \quad (2,9)$$

we transform the function (2,5) as follows:

$$g = \frac{q_1^2 + 3p_1^2}{2} + \frac{q^2}{2} - \frac{p^2}{2} - \frac{p_1^2}{p} - q q_1 \cos(\omega_1 - \omega) + q_1 \cos(\vartheta_1 - \omega_1) \left[ 2p_1 - p - \frac{p_1^2}{p} \right]. \quad (2,10)$$

Effecting the differentiation, we obtain in the final form the system of necessary conditions:

$$q_1 \sin(\vartheta_1 - \omega_1) \left[ 2p_1 - p - \frac{p_1^2}{p} \right] + \lambda_1 [pq \sin(\vartheta_1 - \omega) - p_1 q_1 \sin(\vartheta_1 - \omega_1)] = 0, \quad (2,11)$$

$$\lambda_2 [pq \sin(\vartheta_2 - \omega) - p_2 q_2 \sin(\vartheta_2 - \omega_2)] = 0, \quad (2,12)$$

$$-p + \frac{p_1^3}{p^2} + q_1 \cos(\vartheta_1 - \omega_1) \left[ \frac{p_1^2}{p^2} - 1 \right] + \lambda_1 [2p + q \cos(\vartheta_1 - \omega)] + \lambda_2 [2p + q \cos(\vartheta_2 - \omega)] = 0, \quad (2,13)$$

$$q - q_1 \cos(\omega_1 - \omega) + \lambda_1 p \cos(\vartheta_1 - \omega) + \lambda_2 p \cos(\vartheta_2 - \omega) = 0, \quad (2,14)$$

$$q [-q_1 \sin(\omega_1 - \omega) + \lambda_1 p \sin(\vartheta_1 - \omega) + \lambda_2 p \sin(\vartheta_2 - \omega)] = 0, \quad (2,15)$$

$$p^2 + pq \cos(\vartheta_1 - \omega) - p_1^2 - p_1 q_1 \cos(\vartheta_1 - \omega_1) = 0, \quad (2,16)$$

$$p^2 + pq \cos(\vartheta_2 - \omega) - p_2^2 - p_2 q_2 \cos(\vartheta_2 - \omega_2) = 0. \quad (2,17)$$

The last system consists of seven equations with seven unknowns  $p$ ,  $q$ ,  $\omega$ ,  $\vartheta_1$ ,  $\vartheta_2$ ,  $\lambda_1$ ,  $\lambda_2$ . The equations (2,12), (2,17) & (2,14), (2,15) may respectively substituted by the following ones, considering that in (2,14) and (2,15)  $q \neq 0$  :

$$pq \cos \omega = p_2 q_2 \cos \omega_2 + (p_2^2 - p^2) \cos \vartheta_2, \quad (2,18)$$

$$pq \sin \omega = p_2 q_2 \sin \omega_2 + (p_2^2 - p^2) \sin \vartheta_2, \quad (2,19)$$

$$q \cos \omega = q_1 \cos \omega_1 - p (\lambda_1 \cos \vartheta_1 + \lambda_2 \cos \vartheta_2), \quad (2,20)$$

$$q \sin \omega = q_1 \sin \omega_1 - p (\lambda_1 \sin \vartheta_1 + \lambda_2 \sin \vartheta_2). \quad (2,21)$$

Remark 1.- The multiplier  $\lambda_2$  is  $\neq 0$ . In the opposite case the system of equations (2,11) - (2,17) would break up into two independent groups (2,11) - (2,16) and (2,17). The last equation (2,17) is the condition of flight orbit intersection with the final orbit. As to the first group of equations (2,11) - (2,16), it would define the transition to flight's intermediate orbit with minimum velocity accretion, without any kind of limitations. It may be shown, that such a minimum will be on the flight orbit coinciding with the initial orbit, but this case is excluded from the consideration as being trivial.

Remark 2.- Assume that  $p, q, \omega$  are found. Then the equation (2,17) will give, generally speaking, two values for the angle  $\vartheta_2$ . As to the equation (2,12), it is the condition for the coincidence of these two values, as is easy to verify. Therefore, tangency of the flight orbit with the final one will take place at the point  $\vartheta_2$ , as this should be expected from the purport of the problem set up.

Remark 3.- It follows from the equations (2,11), (2,15) and (2,16) that the tangency of a noncircular flight orbit ( $q \neq 0$ ) with the initial orbit at the point of initial impulse is only possible in the case when the lines of apsides of the three orbits coincide.

### #3. - FLIGHT BETWEEN CIRCULAR AND SMALL ECCENTRICITY ORBITS WITHOUT TAKING INTO ACCOUNT THE TIME OF MOTION

In case of circular boundary orbits

$$q_1 = 0, \quad q_2 = 0. \quad (3,1)$$

From the equations (2,11) and (2,12), we have

$$\sin(\vartheta_1 - \omega) = 0, \quad \sin(\vartheta_2 - \omega) = 0. \quad (3,2)$$

since we are in a position to show that  $\lambda_1 = 0$  does not satisfy the remaining equations. Rejecting the trivial case  $\vartheta_1 = \vartheta_2$ , we obtain from the inequalities (3,2) two possibilities:

$$\vartheta_1 = \omega, \quad \vartheta_2 = \omega + \pi, \quad (3,3)$$

$$\vartheta_1 = \omega - \pi, \quad \vartheta_2 = \omega. \quad (3,4)$$

Let us introduce dual signs: the upper ones for the case (3,3), the lower ones for the case (3,4). The correlations (2,16) and (2,17) will then give

$$p = \sqrt{\frac{p_1^2 + p_2^2}{2}}, \quad q = \pm \frac{p_1^2 - p_2^2}{\sqrt{2(p_1^2 + p_2^2)}}. \quad (3,5)$$

Since  $q > 0$  always, we shall obtain in the case (3,3) the flight from the orbit of lesser radius to that of greater radius, i. e.  $r_2 > r_1, p_1 > p_2$  and the opposite in the case (3,4), i. e.  $r_2 < r_1, p_1 < p_2$ .



The equation (2,15) is satisfied automatically. From the equations (2,13) and (2,14) we find

$$\lambda_1 = \frac{p_2^4 - p_1^3 p}{4p^4}, \quad \lambda_2 = \frac{p_1^3 (p_1 - p)}{4p^4}. \quad (3,6)$$

Passing to Keplerian elements in formulas (3,5), we have:

$$a = \frac{1}{2} (a_1 + a_2), \quad e = \pm \frac{a_2 - a_1}{a_2 + a_1}, \quad (3,7)$$

where indices 1 and 2 denote the respective reference to initial and final orbits.

Therefore, in the given case the Homan ellipse resulted to be the <sup>unique</sup> optimum orbit (with a precision to arbitrary choice of ).

Let us consider now the flight between orbits of small eccentricity, introducing the small parameter, so that

$$q_1 = \varepsilon q'_1, \quad q_2 = \varepsilon q'_2. \quad (3,8)$$

We shall seek the solution of the optimum problem, i. e. the solution of equations (2,11) - (2,17) in the form of series by powers  $\varepsilon$  and retain only the terms of the first order. We shall denote by strokes the coefficients of series at first powers of  $\varepsilon$ , and without strokes - the quantities taken on the Homan ellipse.

By the strength of the system (2,11) - (2,17), and introducing the denotations A, B, R, S, we obtain

$$\dot{\vartheta}_1 - \omega' = \pm \frac{p_1 q_1}{\lambda_1 p q} \sin(\vartheta_1 - \omega_1) \left[ \frac{p}{p_1} + \frac{p_1}{p} + \lambda_1 - 2 \right] = A, \quad (3,9)$$

$$\dot{\vartheta}_2 - \omega' = \mp \frac{p_2 q_2}{p q} \sin(\vartheta_2 - \omega_2) = B, \quad (3,10)$$

$$(2p \pm q) \lambda'_1 + (2p \mp q) \lambda'_2 = \cos(\vartheta_1 - \omega_1) \left[ 1 - \frac{p_1^2}{p^2} \right] q'_1 \mp (\lambda_1 - \lambda_2) q' + \\ + \left( 1 + \frac{2p_1^3}{p^3} - 2\lambda_1 - 2\lambda_2 \right) p' = R, \quad (3,11)$$

$$\pm p \lambda'_1 \mp p \lambda'_2 = \cos(\omega_1 - \omega) q'_1 \mp (\lambda_1 - \lambda_2) p' - q' = S, \quad (3,12)$$

$$\pm \lambda_1 p q (\dot{\vartheta}_1 - \omega') \mp \lambda_2 p q (\dot{\vartheta}_2 - \omega') = q \sin(\omega_1 - \omega) q'_1, \quad (3,13)$$

$$(2p \pm q) p' \pm p q' = p_1 q'_1 \cos(\vartheta_1 - \omega_1), \quad (3,14)$$

$$(2p \mp q) p' \mp p q' = p_2 q'_2 \cos(\vartheta_2 - \omega_2). \quad (3,15)$$

From the equalities (3,9), (3,10) and (3,13) we find

$$\operatorname{tg} \omega = \frac{p_1 q_1' [2(p_1 - p) + \lambda_1 p] \sin \omega_1 - p p_2 q_2' \lambda_2 \sin \omega_2}{p_1 q_1' [2(p_1 - p) + \lambda_1 p] \cos \omega_1 - p p_2 q_2' \lambda_2 \cos \omega_2}. \quad (3,16)$$

The equations (3,14) - (3,15) will give

$$p' = \frac{p_1 q_1' \cos(\vartheta_1 - \omega_1) + p_2 q_2' \cos(\vartheta_2 - \omega_2)}{4p}, \quad (3,17)$$

$$q' = - \frac{p_1 q_1' (q \mp 2p) \cos(\vartheta_1 - \omega_1) + p_2 q_2' (q \pm 2p) \cos(\vartheta_2 - \omega_2)}{4p^2}, \quad (3,18)$$

while from the equations (3,11) and (3,12) we have:

$$\lambda_1' = \frac{pR - (q \mp 2p)S}{4p^2}, \quad \lambda_2' = \frac{pR - (q \pm 2p)S}{4p^2}. \quad (3,19)$$

In the equation obtained by subtraction of equations (2,11) and (2,12) from (2,15), we shall compute the terms of the second order relative to :

$$\alpha \vartheta_1' + \beta \vartheta_2' + \gamma \omega' = C, \quad (3,20)$$

where

$$\begin{aligned} C &= q_1' \left[ \frac{p_1^2 - p^2}{p^2} p' - p_1 \lambda_1' \mp q' \right] \sin(\vartheta_1 - \omega_1) - p_2 q_2' \lambda_2' \sin(\vartheta_2 - \omega_2), \\ \alpha &= p_1 q_1' \left[ \frac{p}{p_1} + \frac{p_1}{p} - 2 + \lambda_1 \right] \cos(\vartheta_1 - \omega_1), \quad \beta = p_2 q_2' \lambda_2' \cos(\vartheta_2 - \omega_2), \\ \gamma &= q q_1' \cos(\omega_1 - \omega). \end{aligned} \quad (3,21)$$

For  $\omega', \vartheta_1', \vartheta_2'$  we shall find from (3,9), (3,10) and (3,20)

$$\omega' = \frac{-\alpha A - \beta B + C}{\alpha + \beta + \gamma}, \quad \vartheta_1' = \omega' + A, \quad \vartheta_2' = \omega' + B. \quad (3,22)$$

Let us now compare the results obtained with those by Lawden [2] from a two-pulse flight between orbits. In this last paper the value of the characteristic velocity of the initial and final impulses (boosts) is minimized. The correction formulas for the eccentricity and the parameter are equivalent, i.e. the shape of the orbit is the same in both flights. In the expressions for  $\operatorname{tg} \omega$  the coefficients standing at trigonometric functions differ from the corresponding coefficients of formula (3,16).

## #4.- MOTION TIME ALONG THE ORBIT

We shall find now the motion time along the orbit as a function of the polar angle  $\vartheta$ . Assume that a polar angle  $\vartheta_1$  corresponds to the time  $t_1$  and a polar angle  $\vartheta_2$  to the time  $t_2$ . We shall introduce the function

$$\psi = K(t_2 - t_1) = \psi(\vartheta_2, \vartheta_1, p, q, \omega), \quad (4.1)$$

where  $K$  is given by the formula (2,6), and  $p, q, \omega$  — by the elements of the orbit considered.

From the surface integral

$$r^2 \frac{d\theta}{dt} = Kp^{-1} \quad (4.2)$$

it is easy to find that

$$\psi = p^{-1} \int_{\vartheta_1 - \omega}^{\vartheta_2 - \omega} \frac{dv}{(p + q \cos v)^2}. \quad (4.3)$$

We shall compute the partial derivatives of the function

$$\frac{\partial \psi}{\partial \vartheta_2} = \frac{1}{p [p + q \cos(\vartheta_2 - \omega)]^2}, \quad \frac{\partial \psi}{\partial \vartheta_1} = -\frac{1}{p [p + q \cos(\vartheta_1 - \omega)]^2}, \quad (4.4)$$

$$\frac{\partial \psi}{\partial \omega} = -\frac{\partial \psi}{\partial \vartheta_2} - \frac{\partial \psi}{\partial \vartheta_1}, \quad (4.5)$$

$$\frac{\partial \psi}{\partial p} = -p^{-2} \int_{\vartheta_1 - \omega}^{\vartheta_2 - \omega} \frac{dv}{(p + q \cos v)^2} - 2p^{-1} \int_{\vartheta_1 - \omega}^{\vartheta_2 - \omega} \frac{dv}{(p + q \cos v)^3}, \quad (4.6)$$

$$\frac{\partial \psi}{\partial q} = -2p^{-1} \int_{\vartheta_1 - \omega}^{\vartheta_2 - \omega} \frac{\cos v}{(p + q \cos v)^3} dv. \quad (4.7)$$

Expanding the function  $\psi$  by powers of eccentricity  $e = \frac{q}{p}$  with a precision to the terms of the first order, we obtain

$$\psi = \frac{\vartheta_2 - \vartheta_1}{p^2} - \frac{2q}{p^2} [\sin(\vartheta_2 - \omega) - \sin(\vartheta_1 - \omega)]. \quad (4.8)$$

We shall find the function  $\psi$  and its derivatives in case of flight along the Homan ellipse. Let  $\vartheta_1$  be the polar angle at time of initial boost, and  $\vartheta_2$  — the polar angle at time of encounter with the final orbit. Then we shall have

.../...

$$\psi = \frac{\pi}{(p^2 - q^2)^{3/2}}, \quad (4,9)$$

$$\left. \begin{aligned} \frac{\partial \psi}{\partial p} &= \frac{1}{p(p^2 - q^2)^{3/2}}, \quad \frac{\partial \psi}{\partial q} = -\frac{1}{p(p^2 - q^2)^{3/2}}, \quad \frac{\partial \psi}{\partial \omega} = \mp \frac{4q}{(p^2 - q^2)^{5/2}}, \\ \frac{\partial \psi}{\partial p} &= -\frac{3p\pi}{(p^2 - q^2)^{5/2}}, \quad \frac{\partial \psi}{\partial q} = \frac{3q\pi}{(p^2 - q^2)^{5/2}}. \end{aligned} \right\} (4,10)$$

#### #5. - SYSTEM OF NECESSARY CONDITIONS IN THE CASE OF FLIGHT TAKING INTO ACCOUNT THE CONCRETE MOTION TIME ALONG ORBITS

We shall consider two material bodies moving along the initial and final orbits. Depending upon the concrete physical problem, we can take for each material body either a rocket, a satellite or a planet. We shall neglect the masses of bodies relative to that of the central body, and also the dimensions of material bodies.

Assume that  $T_1$  is the time of passage through the pericenter on the initial orbit with elements  $p_1, q_1, \omega_1$ ; obviously, at that time the polar angle of the first material body will be  $\omega_1$ . To the moment  $T_2$  of passage through the pericenter over the final orbit with elements  $p_2, q_2, \omega_2$  will correspond the polar angle  $\omega_2$ .

At the time  $t_1$ , when the polar angle is equal to  $\omega_1$ , there takes place a boost (impulse), as a result of which the first material body changes its orbit. At the time  $t_2$ , when the polar angle is  $\omega_2$ , the intermediate orbit of the flight intersects the final orbit, and the material bodies meet.

We must find the flight orbit, i. e. the elements  $p, q, \omega$ , and also the times  $t_1$  and  $t_2$  and the polar angles  $\omega_1, \omega_2$  in such a way, that the value of the characteristic velocity of the initial boost at the time  $t_1$  be minimum.

We shall use the equations (1,13) and (1,15) as the system of necessary conditions with the corresponding substitution of denotations as was done in #2. The expression (2,10) is valid for the function  $g$ . The conditions (2,2) and (2,3) must be fulfilled at elements' discontinuity points. But besides that, it is necessary to add the conditions of motion time coincidence till the encounter of material bodies.

We shall introduce the following denotations :

$$\alpha = K(T_2 - T_1), \quad (5.1)$$

$$\psi_1 = K(t_1 - T_1) = \psi(\vartheta_1, \omega_1, p_1, q_1, \omega_1), \quad (5.2)$$

$$\psi = K(t_2 - t_1) = \psi(\vartheta_2, \vartheta_1, p, q, \omega), \quad (5.3)$$

$$\psi_2 = K(t_2 - T_2) = \psi(\vartheta_2, \omega_2, p_2, q_2, \omega_2). \quad (5.4)$$

From the identity

$$K(t_1 - T_1) + K(t_2 - t_1) - K(t_2 - T_2) - \alpha \equiv 0 \quad (5.5)$$

we shall obtain

$$\psi_3 = \psi_1 + \psi - \psi_2 - \alpha = 0. \quad (5.6)$$

The condition of motion time coincidence may be determined by a different method. Assume that  $t_0$  is a certain moment of time;  $\omega_0$  is the polar angle of the first material body;  $\bar{\omega}$  is the angular distance between the bodies at this time, computed from the first material body. Then it is necessary that

$$\psi(\vartheta_1, \omega_0, p_1, q_1, \omega_1) + \psi(\vartheta_2, \vartheta_1, p, q, \omega) - \psi(\vartheta_2, \omega_0 + \bar{\omega}, p_2, q_2, \omega_2) = 0. \quad (5.7)$$

**Remark 1.-** It is assumed in this work that the encounter of material bodies takes place during the first convolution of flight orbit or that  $\vartheta_2 - \vartheta_1 < 2\pi$ .

**Remark 2.-** The angles  $\vartheta_1, \vartheta_2$  must be measured continuously from the polar axis, and should not be bounded by frames  $[0, 2\pi]$ .

The system of necessary conditions in the final form will be

$$q_1 \sin(\vartheta_1 - \omega_1) \left[ 2p_1 - p - \frac{p_1^2}{p} \right] + \lambda_1 [pq \sin(\vartheta_1 - \omega) - p_1 q_1 \sin(\vartheta_1 - \omega_1)] + \\ + \lambda_2 \left( -\frac{\partial \psi_1}{\partial \vartheta_1} - \frac{\partial \psi}{\partial \vartheta_1} \right) = 0, \quad (5.8)$$

$$\lambda_2 [pq \sin(\vartheta_2 - \omega) - p_2 q_2 \sin(\vartheta_2 - \omega_2)] + \lambda_3 \left( \frac{\partial \psi_2}{\partial \vartheta_2} - \frac{\partial \psi}{\partial \vartheta_2} \right) = 0, \quad (5.9)$$

$$-p + \frac{p_1^3}{p^2} + q_1 \cos(\vartheta_1 - \omega_1) \left[ \frac{p_1^2}{p^2} - 1 \right] + \lambda_1 [2p + q \cos(\vartheta_1 - \omega)] + \\ + \lambda_2 [2p + q \cos(\vartheta_2 - \omega)] + \lambda_3 \frac{\partial \psi}{\partial p} = 0, \quad (5.10)$$

$$q - q_1 \cos(\omega_1 - \omega) + \lambda_1 p \cos(\vartheta_1 - \omega) + \lambda_2 p \cos(\vartheta_2 - \omega) + \lambda_3 \frac{\partial \psi}{\partial q} = 0, \quad (5.11)$$

$$-q q_1 \sin(\omega_1 - \omega) + \lambda_1 p q \sin(\vartheta_1 - \omega) + \lambda_2 p q \sin(\vartheta_2 - \omega) + \lambda_3 \frac{\partial \psi}{\partial \omega} = 0, \quad (5.12)$$

$$p^2 + pq \cos(\vartheta_1 - \omega) - p_1^2 - p_1 q_1 \cos(\vartheta_1 - \omega_1) = 0, \quad (5.13)$$

$$p^2 + pq \cos(\vartheta_2 - \omega) - p_2^2 - p_2 q_2 \cos(\vartheta_2 - \omega_2) = 0, \quad (5.14)$$

$$\psi_1 + \psi - \psi_2 - \alpha = 0. \quad (5.15)$$

The system thus obtained consists of eight equations with eight unknowns:  $\vartheta_1, \vartheta_2, p, q, \omega, \lambda_1, \lambda_2, \lambda_3$ .

#### #6.- FLIGHT BETWEEN CIRCULAR ORBITS TAKING INTO ACCOUNT THE MOTION TIME

In case of circular boundary orbits

$$q_1=0, \quad q_2=0. \quad (6,1)$$

Taking into account (4,8), we shall find

$$\psi_1 = \frac{\vartheta_1 - \omega_1}{p_1^3}, \quad \psi_2 = \frac{\vartheta_2 - \omega_2}{p_2^3}. \quad (6,2)$$

Effecting the substitution of the correlations (6,1) and (6,2) into the system of equations (5,8) — (5,15), we shall find, that it follows from the equation (5,11) that all  $\lambda_1, \lambda_2, \lambda_3$  are not simultaneously equal to zero. That is why the determinant, composed of coefficients at the multipliers  $\lambda_1, \lambda_2, \lambda_3$  in the homogenous equations (5,8), (5,9), (5,12) must be equal to zero. Let us compute the indicated determinant:

$$p^2 q^2 \sin(\vartheta_1 - \omega) \sin(\vartheta_2 - \omega) \left( \frac{\partial \psi}{\partial \omega} + \frac{\partial \psi}{\partial \vartheta_2} + \frac{\partial \psi}{\partial \vartheta_1} + \frac{1}{p_1^3} - \frac{1}{p_2^3} \right) = 0. \quad (6,3)$$

From the correlation (4,5) and the equality (6,3) it follows, that either  $\sin(\vartheta_1 - \omega)$ , or  $\sin(\vartheta_2 - \omega)$  are equal to zero. We shall prove that in both cases

$$\lambda_3 = 0. \quad (6,4)$$

Let us assume the opposite, i.e. that  $\lambda_3 \neq 0$ . Assume that  $\sin(\vartheta_1 - \omega) = 0$ ; then, it follows from the equation (5,8)

$$\frac{1}{p_1^3} = - \frac{\partial \psi}{\partial \vartheta_1} = \frac{1}{p [p + q \cos(\vartheta_1 - \omega)]^2} = \frac{p}{p_1^4},$$

and hence  $p = p_1$ , which is in contradiction with the equation (5,13). Similarly, we may show that (6,4) follows from  $\sin(\vartheta_2 - \omega) = 0$

The equality (6,4) implies that the system of equations (5,8) — (5,15) splits into two groups: (5,8) — (5,14) and (5,15). The first group of equations coincides with the necessary conditions of the optimum

problem without taking into account the motion time (#2) and thus has a unique solution — the Homan ellipse. The equation (5,15) is the condition of motion time coincidence and can always be satisfied by the appropriate choice of angular distance of the pericenter  $\omega$ .

Taking into account the correlations (4,9), (6,2), we have from (5,15)

$$\frac{\vartheta_1 - \omega_1}{p_1^3} + \frac{\pi}{(p^2 - q^2)^{3/2}} - \frac{\vartheta_2 - \omega_2}{p_2^3} - \alpha = 0. \quad (6,5)$$

Let us note that here  $\omega_1$  is the angle, responding to the position of the first material body on the initial orbit at the time  $T_1$ ;  $\omega_2$  is the angle responding to the position of the second material body on the final orbit at the time  $T_2$ . If the boundary orbits have small eccentricities, it is natural to keep for  $\omega_1, \omega_2$  the sense of angular distances of pericenters already in the approximation of the zero order relative to these eccentricities.

Passing to Keplerian elements, it is respectively found in the cases (3,3) and (3,4)

$$\omega = \pi \frac{a_2 \sqrt{a_2 - \left(\frac{a_1 + a_2}{2}\right)^{3/2}}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}} + \frac{\omega_1 a_1 \sqrt{a_1} - \omega_2 a_2 \sqrt{a_2}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}}, \quad (6,6)$$

$$\vartheta_1 = \omega, \quad a_2 > a_1,$$

$$\omega = \pi \frac{a_1 \sqrt{a_1 - \left(\frac{a_1 + a_2}{2}\right)^{3/2}}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}} + \frac{\omega_1 a_1 \sqrt{a_1} - \omega_2 a_2 \sqrt{a_2}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}}, \quad (6,7)$$

$$\vartheta_1 = \omega - \pi, \quad a_2 < a_1.$$

Taking the condition of motion time coincidence in the form (5,7), we would obtain in exactly the same way

$$\omega = \omega_0 + \pi \frac{a_2 \sqrt{a_2 - \left(\frac{a_1 + a_2}{2}\right)^{3/2}}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}} - \tilde{\omega} \frac{a_2 \sqrt{a_2}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}}, \quad (6,8)$$

$$\vartheta_1 = \omega, \quad a_2 > a_1,$$

$$\omega = \omega_0 + \pi \frac{a_1 \sqrt{a_1 - \left(\frac{a_1 + a_2}{2}\right)^{3/2}}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}} - \tilde{\omega} \frac{a_2 \sqrt{a_2}}{a_1 \sqrt{a_1 - a_2} \sqrt{a_2}}, \quad (6,9)$$

$$\vartheta_1 = \omega - \pi, \quad a_2 < a_1.$$

## #7. - PERIOD OF OPTIMUM SITUATIONS' RECURRENCE

It follows from formulas (6,6) and (6,7) that a unique  $\omega$  is to be found for every  $\omega_1, \omega_2$  &  $\alpha$ . We shall take in formula (5,1)

$$T_1 = T_1^0 + n_1 \Pi_1; \quad T_2 = T_2^0 + n_2 \Pi_2 \quad (7,1)$$

where  $\Pi_1, \Pi_2$  are the revolution periods over the initial and final orbits,  $n_1, n_2$  are whole numbers.  $T_1^0, T_2^0$  are certain fixed values of moments of passage time through the pericenters. Therefore, for each  $n_1, n_2$  one may compute  $\omega$  corresponding to them. If the closest moments of time among themselves are chosen for  $T_1$  and  $T_2$ , we shall obtain the least value of  $\omega$  responding to these time moments.

Let us find the variation period of the optimum value (the period of polar angle  $\chi_1$  variation will be the same), which is tantamount to the determination of the time period in the course of which the optimum situation will recur. We shall use the interplanetary flight terminology for the sake of brevity.

We shall analyze the case of circular motion, for example at  $a_2 > a_1$ . We shall continuously vary the initial data in formula (6,8) and see how  $\omega$  will vary. By the strength of the correlations

$$\omega_0 = \omega_{00} + \frac{2\pi}{\Pi_1}(t - t_0), \quad \tilde{\omega} = -\frac{2\pi}{\Pi_s}(t - t_0) + 2n\pi, \quad (7,2)$$

where  $\omega_{00}$  is the initial value of  $\omega_0$ ;  $\Pi_s$  is the synodical revolution period of the finite planet;  $n$  is the number of complete synodical periods, we shall obtain from formula (6,8)

$$\omega = \omega_{00} + \pi \frac{a_2 \sqrt{a_2} - \left(\frac{a_1 + a_2}{2}\right)^{\frac{3}{2}}}{a_1 \sqrt{a_1} - a_2 \sqrt{a_2}} + 2\pi \frac{a_2 \sqrt{a_2}}{a_2 \sqrt{a_2} - a_1 \sqrt{a_1}} n. \quad (7,3)$$

It follows from the last correlation that  $\omega$  has one and only one optimum value in the course of the synodical revolution period of a finite planet.



Let  $t_0$  be the opposition time at  $a_2 > a_1$  or the time of lower conjunction at  $a_1 > a_2$ , and  $\omega_0$  — the planets' polar angle at that moment of time. From (6,8), (6,9) we shall have:

$$\omega = \omega_0 + \pi \frac{a_2 \sqrt{a_2} - \left( \frac{a_1 + a_2}{2} \right)^{3/2}}{a_1 \sqrt{a_1} - a_2 \sqrt{a_2}}, \quad \vartheta_1 = \omega, \quad a_2 > a_1, \quad (7,4)$$

$$\omega = \omega_0 + \pi \frac{a_1 \sqrt{a_1} - \left( \frac{a_1 + a_2}{2} \right)^{3/2}}{a_1 \sqrt{a_1} - a_2 \sqrt{a_2}}, \quad \vartheta_1 = \omega - \pi, \quad a_2 < a_1. \quad (7,5)$$

Thus, the polar angles always differ by a constant angle from the opposition times at times of optimum position of the initial thrust (boost) [ see formulas (7,4), (7,5) ] (or from the moments of lower conjunctions if  $a_1 > a_2$  ). The mean period of optimum situation recurrence is equal to the mean synodical period of revolution of the finite planet.

EXAMPLE.— Let us consider the flight from Earth to Mars. In the astronomical unit system  $a_1 = 1$ ,  $a_2 = 1.524$ , whence  $\omega = -0.525\pi + \omega_0$ , with the angle  $0.525\pi$  corresponding to 96 mean solar days. Thus, at optimum flight to Mars, it is always necessary to take off 96 days before the times of Mars opposition. Such a moment took place on October 31st 1962, since Mars' opposition was on 4 February 1963. The mean period of optimum situation recurrence for the flight to Mars is equal to the mean synodical period of Mars rotation, i. e. 780 mean solar days.

#### #8.- FLIGHT BETWEEN ORBITS OF SMALL ECCENTRICITIES TAKING INTO ACCOUNT THE CONCRETE MOTION TIME

We shall assume that  $q_1$  and  $q_2$  are small. We shall introduce the small parameter  $\varepsilon$  according to formulas (3,11). We shall seek the solution of the optimum problem, i. e. the solution of equations (5,8) — (5,15) in the form of series by powers  $\varepsilon$ . We shall designate by strokes the series' factors at first powers  $\varepsilon$ , and without strokes — the solution on Homan ellipse with the appropriately chosen  $\omega$  (as was done previously (see (6,6)–(6,9)). We shall retain only the terms of the first order of smallness.

Taking into account the correlations (4,8) – (4,10), and introducing the denotations  $\tilde{A}$ ,  $\tilde{B}$ ,  $\tilde{C}$ , we find

$$\vartheta_1 - \omega' = \pm \frac{1}{\lambda_1 p q} \left[ p_1 q_1' \left( \frac{p}{p_1} + \frac{p_1}{p} + \lambda_1 - 2 \right) \sin(\vartheta_1 - \omega_1) + \frac{p_1 - p}{p_1^4} \lambda_3' \right] = \tilde{A}, \quad (8,1)$$

$$\vartheta_2 - \omega' = \mp \frac{1}{\lambda_2 p q} \left[ \lambda_2 p_2 q_2' \sin(\vartheta_2 - \omega_2) + \frac{p - p_2}{p_2^4} \lambda_3' \right] = \tilde{B}, \quad (8,2)$$

$$(2p \pm q) \lambda_1' \mp (2p \mp q) \lambda_2' = \left( 1 + \frac{2p_1^3}{p^3} - 2\lambda_1 - 2\lambda_2 \right) p' \mp (\lambda_1 - \lambda_2) q' + \frac{3p\pi}{(p^2 - q^2)^{3/2}} \lambda_3' \mp \cos(\vartheta_1 - \omega_1) \left[ 1 - \frac{p_1^2}{p^2} \right] q_1', \quad (8,3)$$

$$\pm p \lambda_1' \mp p \lambda_2' = \mp (\lambda_1 - \lambda_2) p' - q' - \frac{3q\pi}{(p^2 - q^2)^{3/2}} \lambda_3' \mp \cos(\omega_1 - \omega) q_1', \quad (8,4)$$

$$\pm \lambda_1 p q (\vartheta_1 - \omega') = \pm \lambda_2 p q (\vartheta_2 - \omega') = \pm \frac{4q}{(p^2 - q^2)^{3/2}} \lambda_3' \mp q q_1' \sin(\omega_1 - \omega), \quad (8,5)$$

$$(2p \pm q) p' \pm p q' = p_1 q_1' \cos(\vartheta_1 - \omega_1), \quad (8,6)$$

$$(2p \mp q) p' \mp p q' = p_2 q_2' \cos(\vartheta_2 - \omega_2), \quad (8,7)$$

$$\frac{p_1 - p}{p_1^4} \vartheta_1' + \frac{p - p_2}{p_2^4} \vartheta_2' \mp \frac{4q}{(p^2 - q^2)^{3/2}} \omega' = \frac{3\pi}{(p^2 - q^2)^{3/2}} (p p' - q q') \mp \frac{2 \sin(\vartheta_1 - \omega_1) q_1'}{p_1^4} - \frac{2 \sin(\vartheta_2 - \omega_2) q_2'}{p_2^4} = \tilde{C}. \quad (8,8)$$

The equations (8,6), (8,7) coincide with the equations (3,14), (3,15), and hence formulas (3,17), (3,18) follow directly for  $p'$ ,  $q'$ . The latter means, that the shape of the flight orbit will be the same as in the case of the problem without taking into account the motion time.

As a consequence of equations (8,1), (8,2) and (8,5), we have

$$\lambda_3' = \frac{p_1 q_1' \left( \frac{p}{p_1} + \frac{p_1}{p} + \lambda_1 - 2 \pm \frac{q}{p_1} \right) \sin(\vartheta_1 - \omega_1) + p_2 q_2' \lambda_2' \sin(\vartheta_2 - \omega_2)}{p_2^{-3} - p_1^{-3}}. \quad (8,9)$$

From the equations (8,1), (8,2) and (8,8) we shall have for

$$\vartheta_1' = \frac{\tilde{A} (p_2^{-3} - p p_1^{-4}) - \tilde{B} (p_2^{-3} - p p_2^{-4}) - \tilde{C}}{p_2^{-3} - p_1^{-3}}, \quad (8,10)$$

$$\vartheta_2' = \frac{\tilde{A} (p_1^{-3} - p p_1^{-4}) - \tilde{B} (p_1^{-3} - p p_2^{-4}) - \tilde{C}}{p_2^{-3} - p_1^{-3}}, \quad (8,11)$$

$$\omega' = \frac{\tilde{A} (p_1^{-3} - p p_1^{-4}) - \tilde{B} (p_2^{-3} - p p_2^{-4}) - \tilde{C}}{p_2^{-3} - p_1^{-3}}. \quad (8,12)$$

Formulas (8,9) — (8,12) and (3,17), (3,18) provide the correction to the Homan ellipse flight orbit in the case when the initial and final orbits have small eccentricities.

Remark.— The initial angle of the pull at initial thrust is not clearly figured in the work. The tangent of this angle may be easily found as the ratio of the radial to transverse velocity accretion component.

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\*\*\*\* THE END \*\*\*\*

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